

Upper Hudson River Sedtran Model Topic 4: Model Development

December 7, 2010

Objectives

- Summarize current model key parameters
 - Sediment classes definition
 - Initial bed properties distribution
 - Incoming sediment Load and composition
- Discuss future refinements to these parameters

Current Model: Sediment Classes

- 1999 Model has two classes and unmovable bed
 - Silt and Clay
 - 90 µm
- 2010 Model defined with 4 classes

Class Limits	<62	62-250	250-2,000	> 2,000
Site Data	27	130-174	546-720	1,645-7,839
Model	30	90	1,500	8,000

Current Model Bed Properties Spatial Distribution

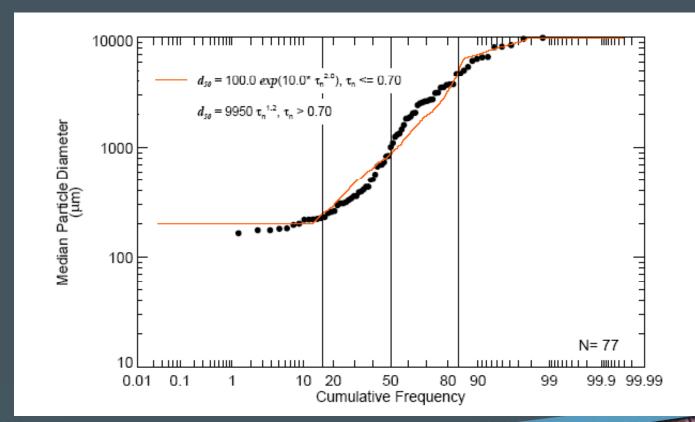
- Non-cohesive bed
 - Use correlation between d_{50} and τ_N
 - d₅₀ from Grain Size Distribution of 0-6" samples
 - τ_N for a 30,000 cfs flow. No significant sensitivity to flow
 - Composition based on correlation between d₅₀ and fsus = f1+f2+f3
 - f1 = 10%, f4 = (1 fsus)
 - f2 and f3 calculated based on the GSD means ratio
- Cohesive bed
 - Average d₅₀ and composition



Current Model

Bed Properties Spatial Distribution

Comparison of predicted and measured distributions of D_{50} in Reach 8 (Figs. 5-10 ~ 5-12 in AQ report)



Current Model: Incoming Load

- Same boundary conditions used in 1999 model
- Hudson River TSS
 - TSS Rating Curve at Fort Edwards incorporating hysteresis
 - Data when available
 - Composition
 - 25% of class 2 based on available USGS data
 - Constant for every flow



Current Model: Incoming Load

- Tributaries TSS
 - Rating Curve for Snook Kill and Moses Kill
 - All other tribs using following procedure:
 - Flow at each tributary was calculated using a flow balance with existing USGS flow gauges and the drainage area of each tributary
 - Annual average load at each tributary was calculated using a Sediment Mass balance between Fort Edwards, Stillwater and Waterford
 - Assume same equation for TSS rating curve
 - Calculate rating curve exponent based to honor annual average load
- Composition also constant except for Moses Kill and direct drainage



Sediment Class Definition

 Refine 4 classes to improve effective particle diameter representation of each range

Class	1	2	3	4
Current	<62 µ	62-250 μ	250-2000 μ	> 2000 µ
Refinement	<62 µ	62-250 μ	250-850 μ	>850 µ

Bed Properties Definition

- Spatial distribution of d₅₀: 2 Approaches
 - 1. Using correlation between d_{50} and τ
 - Easier spatial interpolation
 - 2. Using correlation between d₅₀ and bulk density
 - Makes use of more data
- Spatial distribution of initial composition
 - Use correlations between d₅₀ and fractions

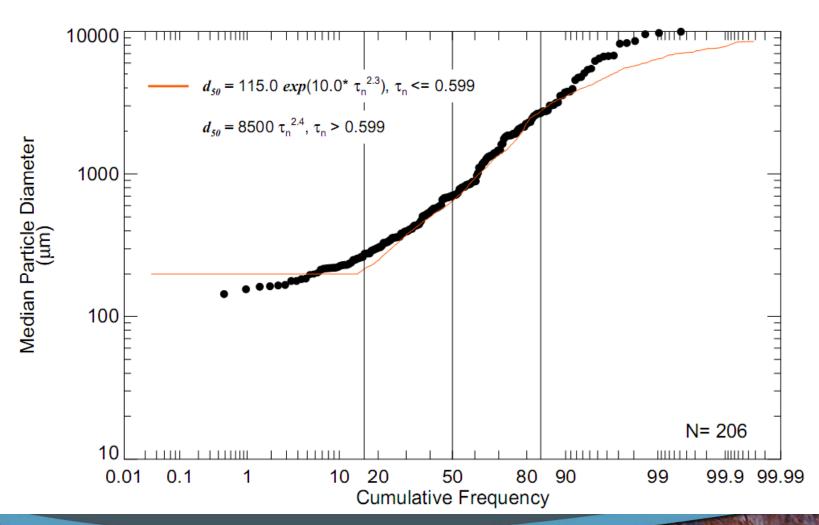


d₅₀ Distribution: Approach 1 Description

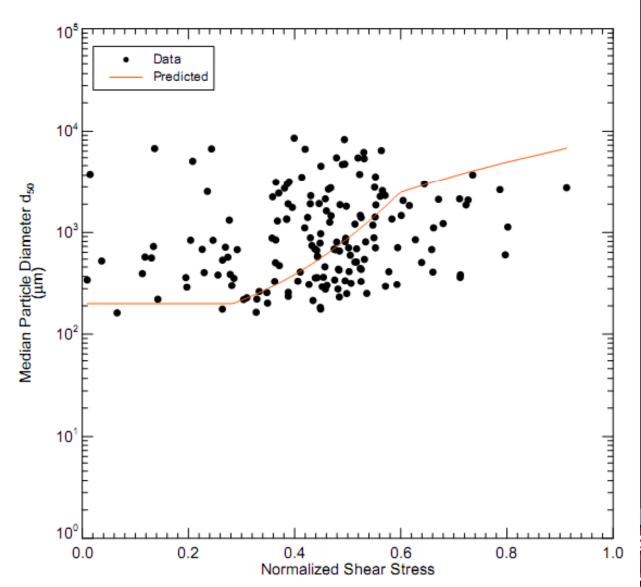
- Use Grain Size Distribution (GSD) obtained for samples from 0-12"
 - About xxx samples for R8
- Reproduce the d_{50} probability distribution using a relationship between normalized τ and d_{50}
- Spread d₅₀ using shear stress in the model domain
- Use data values for cells where samples exist and smooth transition to predicted values



d₅₀ Probability Distribution

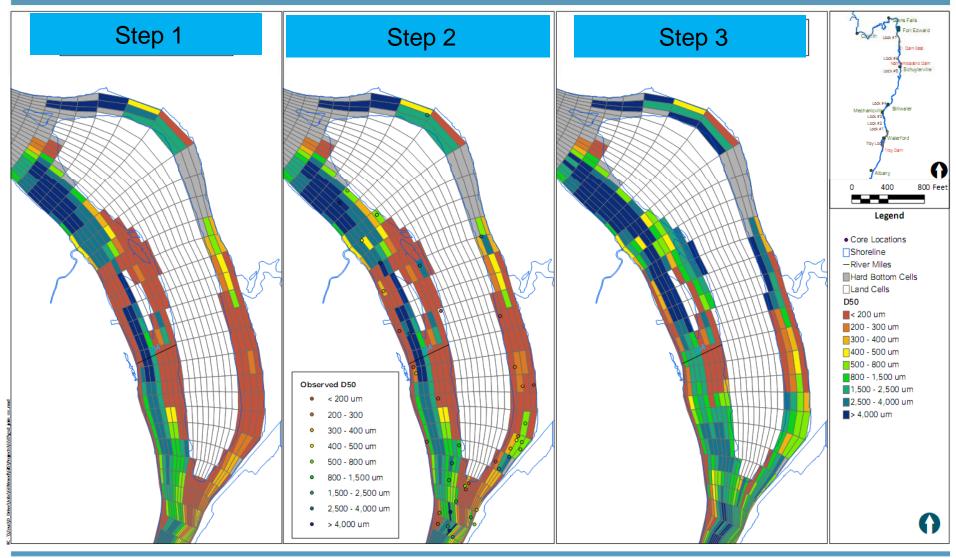


d₅₀ vs Normalized τ

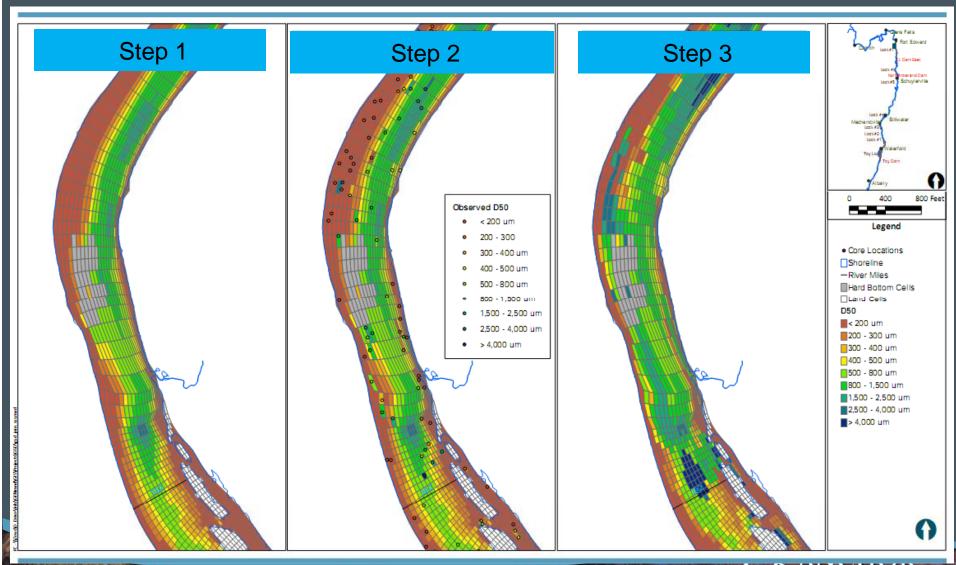




Approach 1 examples



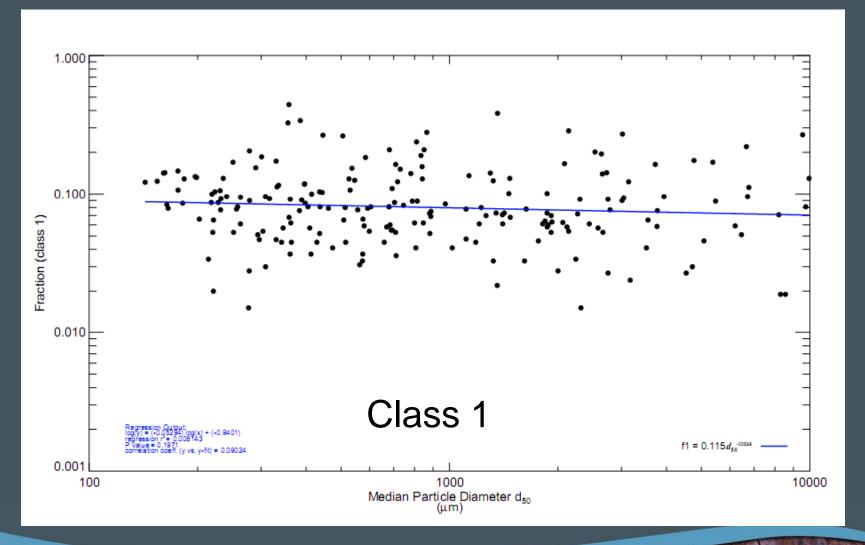
Approach 1 examples

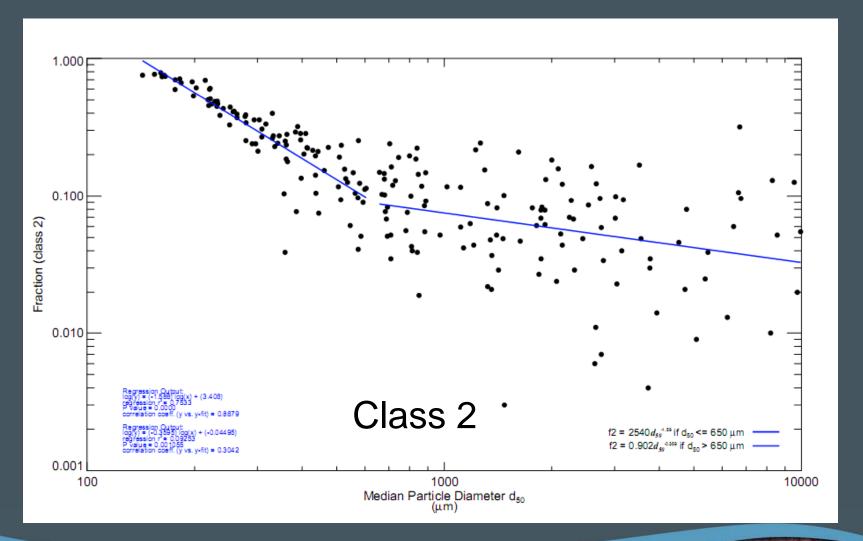


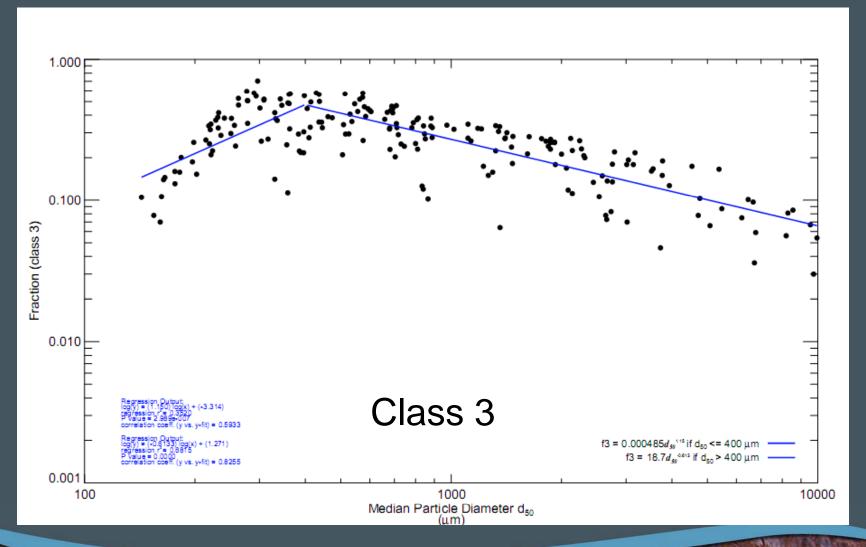


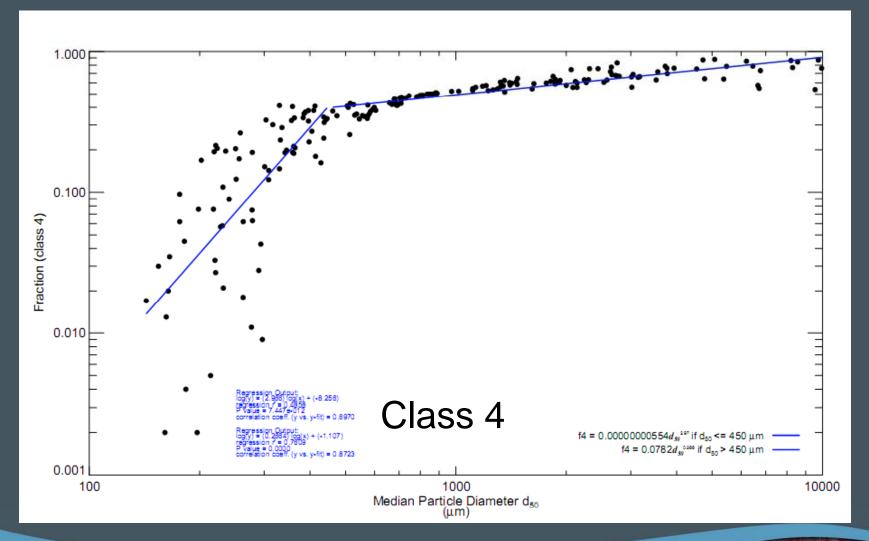
d₅₀ Distribution: Approach 2 Description

• John Wolfe presentation





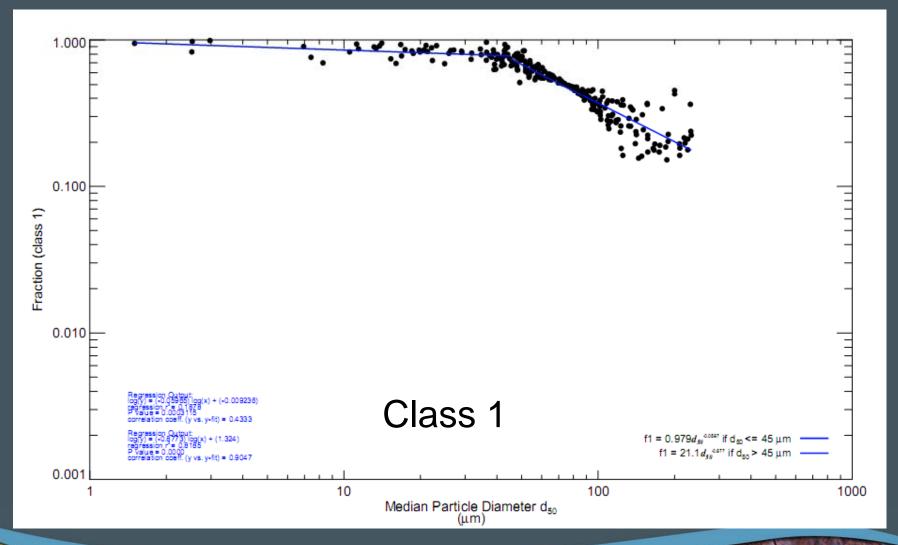




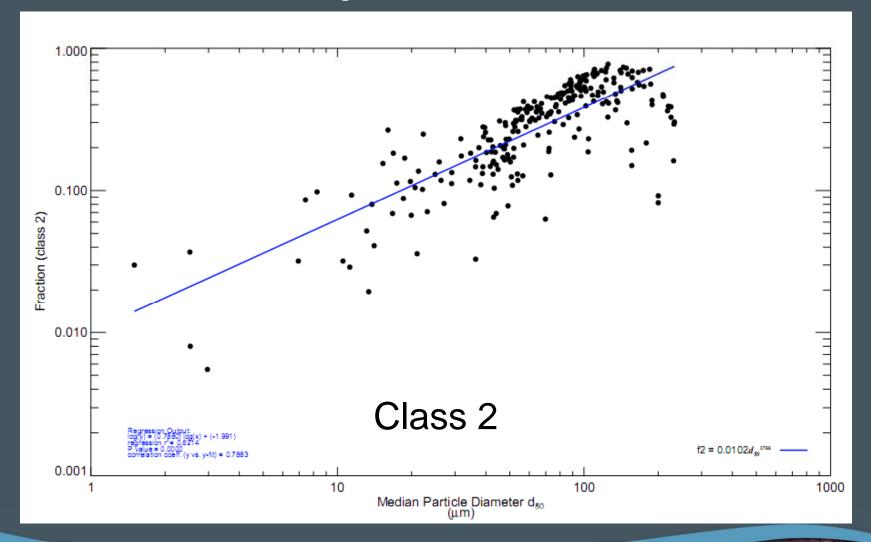


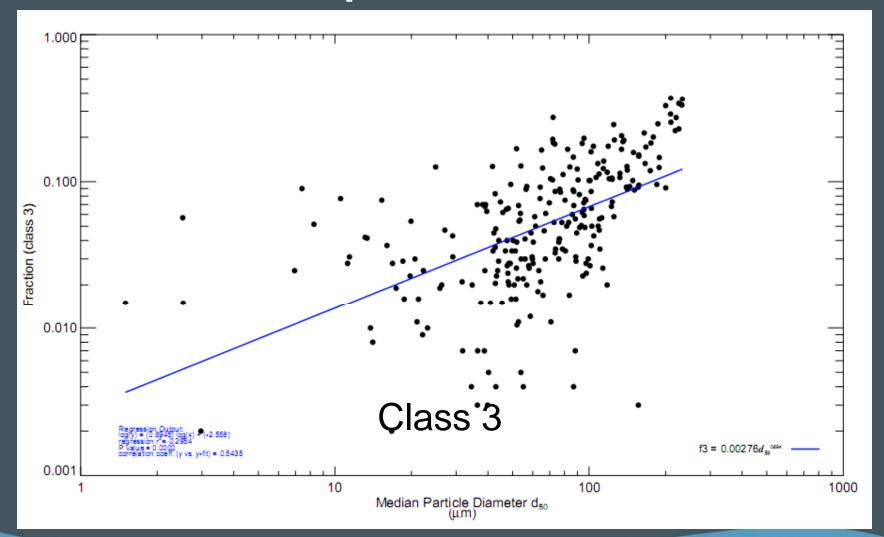
Initial Bed Composition: Proposed Procedure

- Use constant value for Class 1
- For $d_{50} > ~450 \mu$
 - Use correlations to define fractions for Class 3 and Class 4
 - Assign the rest to Class 2
- For $d_{50} < ~450 \mu$
 - Use correlations to define fractions for Class 2 and Class 3
 - Assign the rest to Class 4

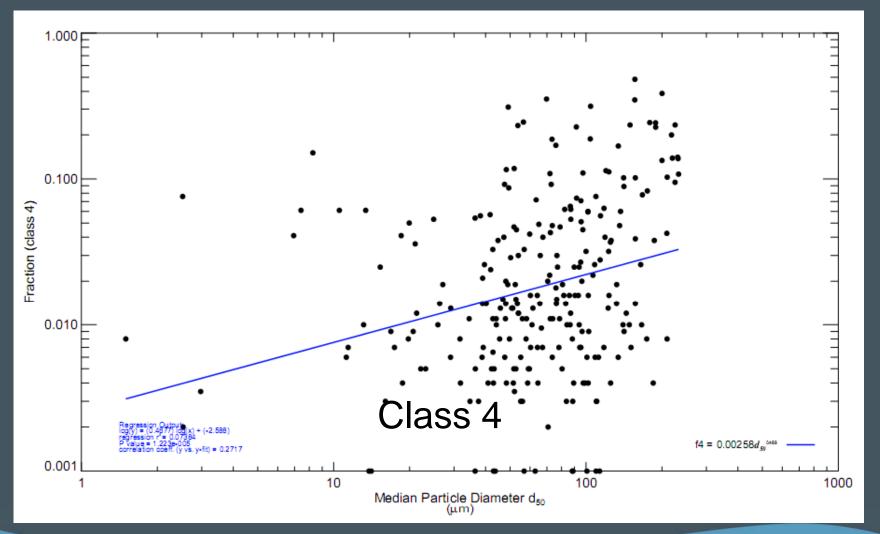










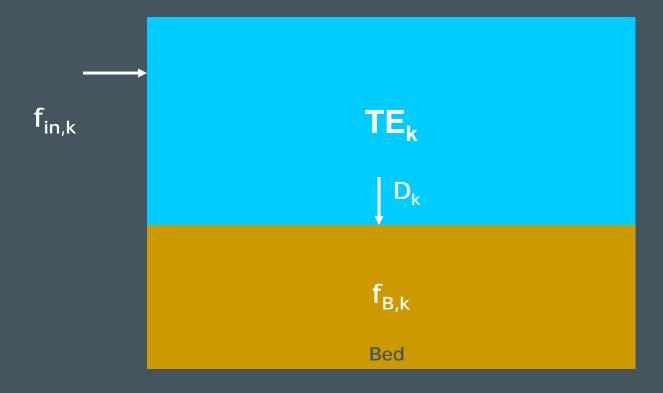




Incoming Load Composition:Proposed Procedure

- 1. Use bed composition and estimates of trapping efficiency of each class to calculate long term average incoming composition
- Generate a rating curve for each incoming class honoring the composition calculated in Step 1

Incoming Load Composition



Incoming Load Composition

• Assuming:
$$f_{B,K} = \frac{D_K}{D_{TOT}}$$
, then

$$F_{IN,K} = (\frac{TE_{TOT}}{TE_K}) f_{B,K}$$

where, $f_{B,K}$ = average bed content for class K

F_{IN.K} = long term average of incoming load for class k

 D_{TOT} = total deposition mass

 D_k = deposition mass for class k

 TE_{TOT} = total trapping efficiency

TE_k = trapping efficiency for class k

Incoming Load Composition

Assuming temporal incoming composition as:

$$f_{IN,K} = \alpha_K \left(\frac{Q}{Q_{cr,k}}\right)^{n_K} \qquad Q > Q_{cr,k}$$

$$= 0 \qquad Q \leq Q_{cr,k}$$

$$=0$$
 $Q \leq Q_{cr}$

• Adjust α and n until:

$$F_{IN,K} = \frac{1}{T} \int_0^T f_{IN,K}(Q) dt$$

Incoming Bed Composition - Example

Target Composition: 80% C1, 14% C2 and 6%C3

